### Hong Kong Housing Authority

### Construction of Housing Authority Public Housing Development at Kai Tak Site 1A and 1B

### Air Ventilation Assessment Detailed Study Report

### 05/2011

	Name	Signature
Prepared & Checked:	S.P. Ma	planting
Reviewed & Approved:	Peter C.T. Lee	Bel En

Version: 3

Date: 31/05/2011

The information contained in this report is, to the best of our knowledge, correct at the time of printing. The interpretation and recommendations in the report are based on our experience, using reasonable professional skill and judgment, and based upon the information that was available to us. These interpretations and recommendations are not necessarily relevant to any aspect outside the restricted requirements of our brief. This report has been prepared for the sole and specific use of our client and AECOM Environment accepts no responsibility for its use by others.

This report is copyright and may not be reproduced in whole or in part without prior written permission.

AECOM Asia Co. Ltd. 11/F, Grand Central Plaza, Tower 2, 138 Shatin Rural Committee Road, Shatin, NT, Hong Kong Tel: (852) 2893 1551 Fax: (852) 2891 0305 www.aecom.com

### Table of Content

### Page

1	INTR	ODUCTION	1
	1.1 1.2 1.3	Background of the Study Objectives Structure of this Report	1 1 1
2	EXPE	ERT EVALUATION	1
	2.1 2.2 2.3	Site Environs Site Wind Environment Site Wind Availability	1 3 5
3	ASSE	ESSMENT METHODOLOGY AND CRITERIA	9
	3.1 3.2 3.3 3.4	General Modelling Tool and Assumptions Wind Velocity Ratio Layout Plan Assessed in this Study	9 9 . 15 . 15
4	KEY	FINDINGS OF AVA STUDY	. 19
	4.1 4.2 4.3 4.4 4.5 4.6	Local Situation Air Ventilation Issues Air Ventilation Improvement Measures Wind Velocity Ratio Results Site Ventilation Assessment Local Air Ventilation Assessment	. 19 . 19 . 19 . 20 . 25 . 25
5	SUM	MARY AND CONCLUSIONS	. 26

### List of Tables

Table 2.1	Frequency of Annual and Summer Season Occurrence of Individual Wind Directions
	at 150mPD

- Table 3.1Grouping of the Overall Test Points
- Table 4.1Summary of Wind Velocity Ratios for Site 1A and Site 1B as a whole under all Sixteen<br/>Wind Directions
- Table 4.2
   Summary of Wind Velocity Ratio for Different Test Point Groups

### List of Figures

- Figure 2.1 Location of the Subject Sites
- Figure 2.2 Topographical Features in Kai Tak Area
- Figure 2.3 Annual Wind Rose from Kai Tak Automatic Weather Station for Year 2004 to 2008
- Figure 2.4 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (North wind direction, 360°)
- Figure 2.5 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (East wind direction, 90°)
- Figure 2.6 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (south wind direction, 180°)
- Figure 2.7 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (west wind direction, 270°)
- Figure 2.8 Wind Roses for Annual and Summer, non-typhoon winds for Kai Tak, corrected to 150mPD at Site 1A & 1B, 1998 2009
- Figure 3.1 Boundaries of Project Area, Assessment Area and Surrounding Area
- Figure 3.2 Extent of Computational Domain adopted in the CFD Model
- Figure 3.3 Example of Cross-sectional Wind Velocity Ratio Vector Plot across the Computational Domain
- Figure 3.4 Images of General Setup in the CFD Model
- Figure 3.5 Images of Grid Cell Setup in the CFD Model
- Figure 3.6 Test Points Selected for this Assessment
- Figure 3.7 Master Layout Plan of the Site 1A
- Figure 3.8 Elevation View of the Site 1A
- Figure 3.10 Elevation Views of Site 1B
- Figure 4.1 Averaged VR<sub>W</sub> Result (Annual)
- Figure 4.2 Averaged VR<sub>W</sub> Result (Summer Season)
- Figure 4.3 Frequency Weighted Wind Velocity Ratio Contour Plot at 2m above Ground

### Appendices

- Appendix A Information extracted from "Experimental Site Wind Availability Study for the Proposed Kai Tak Development, Hong Kong Investigation Report WWTF013-2009"
- Appendix B Details of Predicted Wind Velocity Ratios (VR<sub>W</sub>)
- Appendix C Average VR<sub>w</sub> Result for Individual Test Points and Different Test Points Groups under Different Wind Directions
- Appendix D Wind Velocity Ratio Contour and Vector Plots at 2m above Ground under Different Wind Directions

### HKHA

### 1 INTRODUCTION

### 1.1 Background of the Study

- 1.1.1 A Feasibility Study for Establishment of Air Ventilation Assessment (AVA) System has been completed by the Planning Department in 2005. Since then, the Technical Circular No. 1/06 AVA (the Technical Circular) was jointly issued by the Housing, Planning and Lands Bureau (HPLB) and the Environment, Transport and Works Bureau (ETWB). The Technical Guide for AVA annexed in the Technical Circular detailed the AVA methodology.
- 1.1.2 In response to this Technical Circular which provides guidance for applying AVA to major government projects, the Hong Kong Housing Authority commissioned an AVA study to assess the air ventilation performance at the pedestrian level of the proposed housing development at Kai Tak Site 1A and 1B.

### 1.2 Objectives

- 1.2.1 AECOM is commissioned by the Housing Authority to conduct an AVA detailed study for the public housing development at Kai Tak Site 1A and 1B in accordance with the methodology outlined in the Technical Guide for AVA for Developments in Hong Kong (the Technical Guide) annexed in HPLB and ETWB TC No. 1/06. The main purposes and objectives of the AVA study, echoing the Technical Guide, are:
  - To assess the characteristics of the wind availability (V∞) of the site in detail;
  - To give a general pattern and quantitative estimate of wind performance at the pedestrian level reported using Wind Velocity Ratio (VR); both Site VR (SVR), Local VR (LVR) and wind gust problems are reported where appropriate; and
  - To provide a summary of how the identified problem areas, if any, have been resolved.

### 1.3 Structure of this Report

- 1.3.1 The remainder of the report is organized as follows:
  - Section 2 on expert evaluation and site wind availability;
  - Section 3 on assessment methodology;
  - Section 4 on key findings of AVA detailed study; and
  - Section 5 with summary and conclusions.
- 1.3.2 This AVA study is conducted in two stages using Computational Fluid Dynamic (CFD) model. The first stage covers the Expert Evaluation and the Initial Study which examined the ventilation performance under the 8 most prevailing wind directions (with the percentage of occurrence of the 8 wind directions exceed 75% of time in a typical year). The second stage namely the Detailed Study examined the ventilation performance under all the 16 wind directions. This AVA Report summarizes the findings of the Detailed Study of the AVA study.

### 2 EXPERT EVALUATION

### 2.1 Site Environs

2.1.1 The proposed development is located in the southeastern part of Kowloon Peninsula at the northeastern end of the former Kai Tak Airport. The Subject Sites namely public housing development Kai Tak Sites 1A and 1B are presently an open area within the former Kai Tak Airport North Apron with a total site area of around 9 hectare. It adjoins Road L2, Eastern Road and Kwun Tong Bypass to the east. The location and the environs of the Subject Sites are shown in **Figure 2.1**.





Figure 2.1 Location of the Subject Sites

- 2.1.2 As shown in **Figure 2.1**, to the north of the Subject Sites is the Rhythm Garden, which is a cluster of residential buildings of about 22 to 30 storeys. Further to the north and northwest of Site 1A and Site 1B is mostly characterised by clusters of medium- to high-rise residential and commercial buildings in the San Po Kong area.
- 2.1.3 To the northeast of the Subject Sites are slip roads connecting Kwun Tong Bypass, Prince Edward Road East and Kwun Tong Road. Further northeast of these slip roads are the medium-rise residential buildings in the Choi Hung area.
- 2.1.4 A cluster of residential buildings namely Richland Gardens of about 36-storey high is located along Kwun Tong Bypass to the east of Site 1B together with some adjacent low- to medium-rise buildings of commercial, educational and leisure uses. To the southeast of the Subject Sites are the Kowloon Bay district characterised with clusters of medium-rise commercial and industrial buildings.
- 2.1.5 Proposed educational-use buildings will be standing immediately to the east of Site 1A as well as to the southwest of Site 1B. Further to the south and southwest is now an open area which will be developed into residential sites with building height at about 100 mPD.
- 2.1.6 To the west of the Subject Sites are the planned railway station and Station Square of the Shatin to Central Link. Clusters of mixed-use high-rise buildings are proposed around the Station Square further to the west and northwest.

### 2.2 Site Wind Environment

- 2.2.1 The Subject Sites are located in the south-eastern part of Kowloon Peninsula. As shown in the aerial photo (**Figure 2.2**), the terrain surrounding the Subject Sites is relatively flat with only slightly raised terrain in San Po Kong area to its north and Kowloon Bay area to its southeast. Influence of local topography to the wind flow pattern at the Subject Sites should be minimal.
- 2.2.2 With regards to the local wind condition of the Subject Sites, lower level (16m above mean sea level) wind data are available from the Kai Tak Automatic Weather Station operated by the Hong Kong Observatory. The Kai Tak Automatic Weather Station is located above the roof of the former Kai Tak Airport Fire Station situated at the tip of the ex-Kai Tak Runway.
- 2.2.3 In accordance with the five years (2004 to 2008) annual wind rose from the Kai Tak Automatic Weather Station as shown in **Figure 2.3**, the prevailing winds for years 2004 to 2008 at the lower level of the area are predominantly easterly and southeasterly winds. The annual prevailing winds of the Subject Sites are mainly from the east to southerly east, whereas the summer prevailing winds are mainly coming from the southeast and the southwest quarters (see **Figure 2.8** under **Section 2.3**).
- 2.2.4 Although the influence of local topography to the wind flow pattern around the Subject Sites is minimal, the Subject Sites are surrounded by a number of existing and planned developments in almost all directions. The wind flow pattern at the Subject Sites would be significantly influenced by this surrounding built environment. The annual prevailing winds from the east to southerly east and summer prevailing winds from southerly east towards the Subject Sites would be blocked by the existing medium- to high-rise developments in the Kowloon Bay area. Whereas prevailing summer wind from the southwest towards the Subject Sites is currently unobstructed, but it might be blocked by the future Kai Tak Development. The noise enclosure on Kwun Tong Bypass will also have localised effect on pedestrian level wind speeds.
- 2.2.5 The Subject Sites have to rely on the existing and planned road networks surrounding the Sites as the major breezeways. These include Road L4 running in the southeast-northwest orientation, Road L3 and Kai Yan Street running in the east-west orientation, Prince Edward Road East and Kwun Tong Road running at the north of the Subject Sites and Road L2, Eastern Road, and Kwun Tong Bypass running in the south-north orientation. In addition, open spaces in the proposed Kai Tak Development, such as the North Apron District Park and the Station Square, would also serve as relatively unobstructed air paths for the Subject Sites.



Figure 2.2 Topographical Features in Kai Tak Area



2004 to 2008

### 2.3 Site Wind Availability

- 2.3.1 With reference to the "*Experimental Site Wind Availability Study for the Proposed Kai Tak Development, Hong Kong Investigation Report WWTF013-2009*", Kai Tak Site 1A and Site 1B fall within Study Area B of the Kai Tak Development AVA Study. The wind availability data determined using large scale topographical model (1:2000) tested in a boundary layer wind tunnel under the Kai Tak Development AVA Study for Study Area B were therefore adopted for this AVA detailed study for Kai Tak Site 1A and 1B. The coverage of Study Area B and the relevant wind availability data are extracted and shown in **Appendix A**.
- 2.3.2 The wind tunnel testing techniques used for the site wind availability study satisfied the quality assurance requirements stipulated in the Australasian Wind Engineering Society Quality Assurance Manual, AWES-QAM-1-2001 (2001) and the American Society of Civil Engineers Manual and Report on Engineering Practice No. 67 for Wind Tunnel Studies of Buildings and Structures (1999). The site wind availability study was also conducted in accordance with the recommendations of Planning Department's Feasibility Study for Establishment of Air Ventilation Assessment System Final Report (2005) and Technical Guide for Air Ventilation Assessment for Developments in Hong Kong (2006).
- 2.3.3 The site wind availability study was conducted using a 1:2000 scale topographical model to determine the effects of surrounding topography and urban environment on mean wind speeds and turbulence intensities above the Study Area B.
- 2.3.4 The wind tunnel testing results were subsequently combined with a statistical model of the Kai Tak non-typhoon wind climate, based on wind speed measurements taken at the Kai Tak Automatic Weather Station to determine directional wind characteristics and availability for the Kai Tak Area.
- 2.3.5 Photographs of the 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section for Study Area B under north, east, south and west directions are shown in **Figure 2.4** to **Figure 2.7** for reference.
- 2.3.6 Based on the findings of the site wind availability study, the annual prevailing non-typhoon winds at Kai Tak are mainly coming from the south-east quadrant while from south-east and south-west quadrants during summer months (June to August). The site wind availability study also pointed out that significant reductions in the magnitudes of wind speed were measured at elevations below 150 mPD for N, NNE, NE, ENE and E wind directions caused by the mountains to the north and north-east of the Kai Tak Area. Besides, the mountains located on Hong Kong Island would reduce wind speeds from the south and south-westerly directions. Winds approaching from the south-east were the least affected due to the relatively open water of the Victoria Harbour and Lei Yue Mun.
- 2.3.7 The annual and summer wind roses at 150 mPD based on the results of the site wind availability study are shown in **Figure 2.8**. The wind rose result indicates the dominance of each of the 16 wind directions and distribution of the wind speed at 150m above terrain. The percentage of annual and summer season occurrence of a particular wind direction at level 150 mPD is also presented in **Table 2.1**.



Figure 2.4 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (North wind direction, 360°)



Figure 2.5

1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (East wind direction, 90°)





Figure 2.6 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (south wind direction, 180°)



Figure 2.7 1:2000 scale topographical model of the proposed Kai Tak Development in the low speed test section, Study Area B, (west wind direction, 270°)



Figure 2.8 Wind Roses for Annual and Summer, non-typhoon winds for Kai Tak, corrected to 150mPD at Site 1A & 1B, 1998 - 2009

Table 2.1	Frequency of	Annual	and	Summer	Season	Occurrence	of	Individual
	Wind Direction	is at 150	mPD					

Wind Direction	% of Annual Occurrence	% of Summer Season Occurrence
0° (N)	3.5%	0.8%
22.5º (NNE)	2.4%	0.3%
45º (NE)	5.0%	0.6%
67.5º (ENE)	3.5%	0.8%
90° (E)	17.5%	8.3%
112.5º (ESE)	19.2%	11.4%
135º (SE)	13.9%	19.0%
157.5º (SSE)	9.6%	8.9%
180º (S)	3.0%	6.9%
202.5º (SSW)	2.8%	7.6%
225º (SW)	3.2%	7.2%
247.5º (WSW)	4.6%	12.7%
270° (W)	3.4%	8.4%
292.5º (WNW)	2.3%	4.0%
315º (NW)	2.8%	1.7%
337.5º (NNW)	3.4%	1.4%

### 3 ASSESSMENT METHODOLOGY AND CRITERIA

### 3.1 General

3.1.1 This AVA study is carried out in accordance with the guidelines stipulated in the Technical Guide for AVA for Developments in Hong Kong with regards to CFD modelling. Reference is also made to the "Recommendations on the use of CFD in Predicting Pedestrian Wind Environment" issued by a working group of the COST action C14 "Impact of Wind and Storms on City Life and Built Environment" (COST stands for the European Cooperation in the field of Scientific and Technical Research). COST action C14 is developed by the European Laboratories/Institutes dealing with wind and/or structural engineering, whose cumulative skills, expertise and facilities have an internationally leading position. Thus, it is considered that the COST action C14 is a valid and good reference for CFD modelling in AVA study.

### 3.2 Modelling Tool and Assumptions

- 3.2.1 Assessment was conducted by means of 3-dimensional CFD model and using wind profile information obtained from the site wind availability study discussed in **Section 2.3** above.
- 3.2.2 The well-recognised commercial CFD package FLUENT was used in this exercise. FLUENT model had been widely applied for various AVA research and studies worldwide. The accuracy level of the FLUENT model was very much accepted by the industry for AVA application.
- 3.2.3 <u>Wind Directions</u>: In the CFD model, all 16 wind directions together with their respective % of occurrence determined for the Subject Sites were adopted for simulation of air ventilation performance (see **Table 2.1**)
- 3.2.4 <u>Vertical Wind Profile</u>: Wind environment under different wind directions was defined in the CFD environment. The wind profiles for the 16 wind directions follow those determined from the site wind availability study as extracted in **Appendix A**.
- 3.2.5 <u>Turbulence Model</u>: As recommended in COST action C14, realizable K-epsilon turbulence model was adopted in the CFD model to simulate the real life problem. Common computational fluid dynamics equations are adopted in the analysis.
- 3.2.6 Variables including fluid velocities and fluid static pressure were calculated throughout the domain. The CFD code captures, simulates and determines the air flow inside the domain under study based on viscous fluid turbulence model. Solutions were obtained by iterations.
- 3.2.7 Computational Domain: The 3-dimensional CFD model was constructed to capture all major components such as topographical features and buildings within and in the vicinity of the Subject Sites that would likely affect the wind flow. The methodology described in the Technical Guide was adopted for this assessment. According to the Technical Guide, the surrounding area up to a perpendicular distance of 2 times of the maximum building height within the Subject Sites (2H) is included in the CFD model. The maximum height of building block for the proposed Site 1A and Site 1B developments is around 120mPD. Therefore, a study area covering not less than 240m from the Subject Sites boundary was included in the formulation of the CFD model and is further extended to include some prominent buildings just outside 240m of the Subject Sites boundary. The size of the CFD model for this Study is approximately 4,700 m (L) x 3,500 m (W) x 720 m (H) and contains about 6,500,000 cells. Figure 3.1 shows the boundaries of the Project Area, Assessment Area and Surrounding Area examined in this AVA whereas Figure 3.2 shows the extent of the computational domain adopted in the CFD model. An example cross-sectional wind velocity ratio vector plot across the computational domain under one wind direction is shown in Figure 3.3 and Figure 3.4 shows some images of the general setup in the CFD model.

3.2.8 Given the large computational domain adopted in this assessment and the physical limitation on the computational resources of the CFD model, the horizontal grid size employed in the CFD model in the vicinity of the Project Area was taken as a global general minimum size of about 3m (smaller grid size was also employed for specific fine details including elevated road, proposed car park, etc) and increased for the grid cells further away from the Project Area. Besides, prism cells (each layer of not more than 0.5m thick) were employed above the terrain so that the pedestrian level test points (located at 2m above ground level) were located at least the third cell away from the terrain to ensure a better resolution of flow close to the ground as per the recommendation of COST action C14. **Figure 3.5** shows the images of the grid cell setup in the CFD model.



Figure 3.1 Boundaries of Project Area, Assessment Area and Surrounding Area



Figure 3.2 Extent of Computational Domain adopted in the CFD Model





(View 1)



(View 2)







Figure 3.4 Images of General Setup in the CFD Model



(View 1)



(View 2)









Images of Grid Cell Setup in the CFD Model

- 3.2.9 <u>Test Points</u>: Both perimeter test points and overall test points were selected within the Assessment Area in order to assess the impact on the immediate surroundings and local areas respectively. Perimeter test points were selected along the boundary of the Project Area with separation distance of about 35m. Overall test points were evenly distributed over surrounding open spaces, streets, landscape deck, podium and other parts of the Assessment Area where pedestrian can or will mostly access. All test points are elevated at 2m above ground.
- 3.2.10 The selected overall test points were grouped based on the land use / sensitive receivers as shown in **Figure 3.6** and summarized in **Table 3.1** for ease of discussion. There are 49 perimeter test points (with prefix "P") and 79 overall test points (with prefix "T") selected for the purpose of this AVA study. For test points along the roads, they are located along the footpath on either side of the road.



Group	Description	Test Points
G1	Wang Kwong Road	T1 to T5
G2	Eastern Road, Planned Road L2 and under the Kwun Tong Bypass	T6 to T15 & T27
G3	Corridor along Planned Road L3	T16 – T18
G4	Wang Chiu Road	T19 – T22
G5	Corridor along Planned Road L4	T23 – T27
G6	Planned Shatin to Central Link Station with commercial facility, open space (Station Square) and other specified uses area	T28 to T31
G7	Planned commercial and other specified uses area at Kai Tak Development Area (between Site 1A and Prince Edward Road East)	T32 to T36
G8	Planned commercial and residential development at Kai Tak Development Area 1G	Т37 – Т39
G9	Open space within Project Area of Site 1A	T40 to T46
G10	Open space within Project Area of Site 1B	T47 to T53
G11	Planned schools between Site 1A and Eastern Road	T54 to T56
G12	Planned schools between Site 1B and Road L4	T57 to T60
G13	Planned residential development at Kai Tak Development Area 1H & 1I	T61 to T65
G14	Open space bounded by Choi Hung Estate, Eastern Road and Wang Chiu Road	T66 to T71
G15	Richland Gardens and the adjacent uses to the east of Site 1B	T72 to T79

### Table 3.1 Grouping of the Overall Test Points

### 3.3 Wind Velocity Ratio

- 3.3.1 The wind velocity ratio VR<sub>W</sub> is the frequency weighted wind velocity ratio calculated based on the frequency of occurrence of the eight wind directions selected in the Initial Study or the 16 wind directions examined in the Detailed Study.
- 3.3.2 For the Site Air Ventilation Assessment, the Site Spatial Average Wind Velocity Ratio (SVR<sub>W</sub>) of all perimeter test points are reported. SVR<sub>W</sub> is the average of VR<sub>W</sub> of all perimeter test points.
- 3.3.3 For the Local Air Ventilation Assessment, the Local Spatial Average Wind Velocity Ratio (LVR<sub>w</sub>) of all overall test points and perimeter test points, and individual VR<sub>w</sub> of the overall test points are reported. LVR<sub>w</sub> is the average of all overall test points and perimeter test points.
- 3.3.4 The SVR<sub>W</sub> and LVR<sub>W</sub> are worked out so as to understand the overall impact of air ventilation on the immediate and further surroundings of the Project Area due to the proposed development.

### 3.4 Layout Plan Assessed in this Study

- 3.4.1 The Subject Sites of this AVA Detailed Study covered both Site 1A and Site 1B with about 9 ha in area consisting commercial block, carport block, kindergarten, ground-level retail shops and necessary supporting facilities.
- 3.4.2 The layout plan and elevation of Site 1A is shown in **Figure 3.7** and **Figure 3.8** below.



Figure 3.7 Master Layout Plan of the Site 1A



**Elevation View of the Site 1A** Figure 3.8

3.4.3 The proposed scheme of Site 1B examined in this Detailed Study comprises of nine residential building blocks, commercial facilities, kindergarten and a carport building. The layout plan and elevations are shown in **Figure 3.9** and **Figure 3.10** respectively.



Figure 3.9 Master Layout Plan of the Site 1B



Figure 3.10 Elevation Views of Site 1B

### 4 KEY FINDINGS OF AVA STUDY

### 4.1 Local Situation

4.1.1 The local situation including the site environs, site wind environment, and site wind availability of the Subject Sites are described in **Section 2** above.

### 4.2 Air Ventilation Issues

- 4.2.1 As discussed in **Section 2** above, the terrain surrounding the Subject Sites is relatively flat and influence of local topography to the wind flow pattern at the Subject Sites should be minimal. However, the Subject Sites will be surrounded by a number of existing and planned developments in almost all directions in future, the wind flow pattern at the Subject Sites would be significantly influenced by this surrounding built environment.
- 4.2.2 For example, the annual prevailing winds and summer prevailing winds from the east and the east-southerly east towards the Subject Sites would be partially blocked by the existing medium- to high-rise developments in the Kowloon Bay area such as Richland Gardens and Kowloon Bay industrial buildings. Whereas the prevailing summer wind from the west-southerly west towards the Subject Sites is currently unobstructed, but it might be blocked by other developments of the planned Kai Tak Development.
- 4.2.3 Since the prevailing winds blowing from east to southerly-east covered more than 50% annually, it is important to incorporate wind corridor(s) through and across the Subject Sites along these prevailing wind directions such that acceptable ventilation performance within the Subject Sites could be achieved and at the same time the impact on ventilation to the surrounding existing and planned developments could be minimized.
- 4.2.4 Besides, although northerly and southerly winds are not the prevailing winds in the area. the existing Eastern Road, Kwun Tong Bypass and planned Road L2 serve as the major breezeways for north-south wind movement in the vicinity of the Subject Sites.

### 4.3 Air Ventilation Improvement Measures

4.3.1 During the development of the design schemes for Site 1A and Site 1B, a number of ventilation improvement measures have been incorporated into the building design to enhance air ventilation performance. The incorporated ventilation improvement measures are summarised below:

### Site 1A

- a) Provision of openings at ground level of domestic blocks and commercial centre to improved wind flow at pedestrian level;
- b) The carpark is half-sunken to reduce obstruction to airflow; and
- c) The building separation has been optimized by rotating the wings of the domestic blocks to enhance ait permeability.

### Site 1B

- a) Reduce the number of residential blocks from 10 blocks to 9 blocks;
- b) Building wings at ground floor are strategically opened up to allow wind passage and breezeway at the pedestrian level;
- c) The retail shops at ground level along the north boundary of the site are split to allow air passage to/from the courtyard area of the site;
- d) Align building blocks along with prevailing wind direction;

- e) Streamlined the edge of kindergarten and the north-east corner of retail shops to enhance movement of wind flow; and
- f) Maximize wind permeability of carport structure to allow upwind passage.

### 4.4 Wind Velocity Ratio Results

4.4.1 The annual and summer SVR<sub>W</sub> and LVR<sub>W</sub> for Site 1A and Site 1B are summarized in Table
 4.1. The detailed wind velocity ratios at different test points under all 16 wind directions are presented in Appendix B.

### Table 4.1Summary of Wind Velocity Ratios for Site 1A and Site 1B as a whole<br/>under all Sixteen Wind Directions

	Wind Velo	city Ratios
	Annual	Summer
Perimeter Test Point VRw	0.063 - 0.314	0.061 – 0.285
Overall Test Point VRw	0.061 – 0.382	0.068 – 0.371
SVRw	0.172	0.175
LVRw	0.183	0.185

4.4.2 The results of VR<sub>W</sub> for different groups of test points are summarized in **Table 4.2**.

				Averag	je VR <sub>w</sub>
Group	Description	Test Points	Test Points Level	Annual	Summer
G1	Wang Kwong Road	T1 to T5	Pedestrian Level	0.294	0.299
G2	Eastern Road, Planned Road L2 and under the Kwun Tong Bypass	T6 to T15 & T27	Pedestrian Level	0.256	0.245
G3	Corridor along Planned Road L3	T16 – T18	Pedestrian Level	0.228	0.234
G4	Wang Chiu Road	T19 – T22	Pedestrian Level	0.149	0.116
G5	Corridor along Planned Road L4	T23 – T27	Pedestrian Level	0.205	0.201
G6	Planned Shatin Central Link Station with commercial facility, open space (Station Square) and other specified uses area	T28 to T31	Pedestrian Level	0.134	0.161
G7	Planned commercial and other specified uses area at Kai Tak Development Area (between Site 1A and Prince Edward Road East)	T32 to T36	Pedestrian Level	0.198	0.181
G8	Planned commercial and residential development at Kai Tak Development Area 1G	T37 – T39	Pedestrian Level	0.184	0.195
G9	Open space within Project Area of Site 1A	T40 to T44; T45 to T46	Pedestrian Level; Podium Deck	0.140	0.152
G10	Open space within Project Area of Site 1B	T47 to T51; T52 to T53	Pedestrian Level; Podium Deck	0.169	0.166
G11	Planned schools between Site 1A and Eastern Road	T54 to T56	Pedestrian Level	0.146	0.138
G12	Planned schools between Site 1B and Road L4	T57 to T60	Pedestrian Level	0.139	0.157
G13	Planned residential development at Kai Tak Development Area 1H & 1	T61 to T65	Pedestrian Level	0.186	0.208
G14	Open space bounded by Choi Hung Estate, Eastern Road and Wang Chiu Road	T66 to T71	Pedestrian Level	0.204	0.184
G15	Richland Garden and the adjacent	T72 to T79	Pedestrian Level	0.107	0.111

### Table 4.2 Summary of Wind Velocity Ratio for Different Test Point Groups

4.4.3 The averaged VR<sub>W</sub> result for individual test points and test point groups for annual and the summer season are also presented in the form of bar chart as shown in **Figure 4.1** and **4.2** respectively. The averaged VR<sub>W</sub> result for individual test points and test points in the form of bar chart under the sixteen assessed wind directions are shown in **Appendix C**.

uses to the east of Subject Site 1B

4.4.4 Contour plots of wind velocity ratio at 2m above the pedestrian level of assessment area under the sixteen assessed wind directions are shown in **Appendix D**. The contour plot of the frequency weighted wind velocity ratio at 2m above ground is shown in **Figure 4.3** below.



(a) Perimeter Test Points



(b) Overall Test Points



Figure 4.1 Averaged VR<sub>w</sub> Result (Annual)











Figure 4.2 Averaged VR<sub>w</sub> Result (Summer Season)



Figure 4.3 Frequency Weighted Wind Velocity Ratio Contour Plot at 2m above Ground

### 4.5 Site Ventilation Assessment

- 4.5.1 The predicted annual SVR<sub>w</sub> for Site 1A and Site 1B as a whole is 0.172 under all sixteen wind directions. As shown in **Figure 4.1a**, the predicted annual wind velocity ratio of 28 out of 49 perimeter test points exceeds 0.15 whereas 13 out of 49 perimeter test points exceeds 0.20. During summer season, the predicted summer SVR<sub>w</sub> is 0.175. As indicated in **Figure 4.2a**, wind velocity ratio of 32 out of 49 and 15 out of 49 perimeters test points exceeds 0.15 and 0.20 respectively during summer season.
- 4.5.2 The SVR<sub>W</sub> indicates how the lower portion of the buildings on the project site may affect the wind environment of its immediate vicinity. As discussed in **Section 4.3** above, both Site 1A and Site 1B have incorporated ventilation improvement design into the lower portion of the development including the provision of openings at ground level of domestic blocks and to optimize building separation by rotating the wings of the domestic blocks, etc.
- 4.5.3 Besides, the wind velocity ratio contour plots shown in **Figure 4.3** and **Appendix D** do not indicate any spot within Site 1A and Site 1B which are subject to high wind velocity gradient, wind gust problem within Site 1A and Site 1B is therefore not expected.

### 4.6 Local Air Ventilation Assessment

- 4.6.1 The averaged LVR<sub>w</sub> for Site 1A and Site 1B under annual and summer winds are 0.183 and 0.185 respectively. As shown in **Figure 4.1c** and **Figure 4.2c**, the averaged VR<sub>w</sub> for most test points groups are close to or above 0.15 except Group 15 for annual wind probability data and Group 4 and Group 15 for summer season.
- 4.6.2 Test points for Group 4 and Group 15 are at Wang Chiu Road, Richland Gardens and some existing schools. The reason for the lower averaged VR<sub>W</sub> at these two Groups in both annual and summer season is due to the sheltering effect by its own building structure as well as the prevailing southeasterly wind is obstructed by the massive buildings of the adjacent Kai Yip Estate. This can be illustrated by the relatively higher VR<sub>W</sub> at Point T79 in the same area which is not obstructed by Kai Yip Estate.

### 5 SUMMARY AND CONCLUSIONS

- 5.1.1 This AVA Study Report aims at assessing the characteristics of the wind availability of the site, providing a general pattern and a quantitative estimate of wind performance at the pedestrian level under different wind directions.
- 5.1.2 The ventilation improvement designs that have been incorporated into Site 1A and Site 1B to improve the penetration of wind across the developments include the introduction of building openings at ground level of domestic blocks for Site 1A and Site 1B, streamlined north-east edge of retail shops and kindergarten of Site 1B, deletion of one domestic block at Site 1B, half-sunken design of carpark at Site 1A and reduction of footprint for the carport at Site 1B.
- 5.1.3 To conclude, the air ventilation performance of Site 1A and Site 1B as a whole is considered as acceptable after examined the frequency weighted site and local spatial average wind velocity ratios based on the wind profile and frequencies of all sixteen incoming wind directions.

APPENDICES

Appendix A

Information extracted from "Experimental Site Wind Availability Study for the Proposed Kai Tak Development, Hong Kong - Investigation Report WWTF013-2009" --Appendix A Information extracted from "Experimental Site Wind Availability Study for the Proposed Kai Tak Development, Hong Kong - Investigation Report WWTF013-2009"



НКНА

The Hong Kong University of Science and Technology

•

CLP Power Wind/Wave Tunnel Facility

ation (mPD)	Normalised mean wind speed	Turbulence intensity (%)
25	0.45	20.8%
50	0.47	21.4%
75	0.49	22.1%
100	0.51	22.1%
150	0.57	21.1%
200	0.63	19.7%
300	0.75	14.1%
400	0.84	10.1%
500	0.89	9%0 9

f Shidy Area B 117 5° Aprictio Table B5: Site wind char

U

135° Table B6: Site

400 0.89 0.89	Turbulence intensity (%) 11.8% 11.4% 10.9% 9.5% 8.7% 6.1% 6.1%	Normalised mean wind speed 0.60 0.67 0.71 0.71 0.76 0.76 0.76 0.79 0.89	zatic contrype scale evation (mPD) 25 50 50 75 100 100 150 150 200 300 300 400 100 100 100 100 100 100 100 100 1
	100 3	0.00	200
C0.0 000	7.4%	0.85	300
200 0.02	8.7%	0.79	200
200 0.79 200 0.79	9.5%	0.76	150
150 0.76 200 0.79 200 0.79	10.4%	0.71	100
100 0.71 150 0.76 200 0.79 200 0.79	10.9%	0.67	75
75         0.67           100         0.71           150         0.76           200         0.79           200         0.79	11.4%	0.64	50
50         0.64           75         0.67           100         0.71           150         0.71           200         0.79           200         0.79	11.8%	0.60	25
25         0.60           50         0.64           75         0.67           100         0.71           150         0.76           200         0.79	Turbulence intensity (%	Normalised mean wind speed	totype scale ation (mPD)

0.43 25.0	0.45 24.9	0.49 23.8'	0.54 22.6	0.62 18.9	0.68 17.0	0.76 14.2'
75	100	150	200	300	400	500

The Hong Kong University of Science and Technology

CLP Power Wind/Wave Tunnel Facility

•

AECOM Asia Co. Ltd.

The Hong Kong University of Science and Technology

•

CLP Power Wind/Wave Tunnel Facility

\_

60

59

TABULATED RESULTS FOR KAI TAK-STUDY AREA B APPENDIX B

rototype scale evation (mPD)	Normalised mean wind speed	Turbulence intensity (%
25	0.47	22.1%
50	0.51	21.6%
75	0.53	21.7%
100	0.56	21.3%
150	0.61	20.4%
200	0.64	19.6%
300	0.77	17 50%

### Table B2: Site wind characteristics of Study Area B, 45°

14.2% 10.6%

0.82

400 500

	1 1 1	
ototype scale	Normalised mean	Turbulence
vation (mPD)	wind speed	intensity (%)
25	0.49	24.0%
50	0.53	22.9%
75	0.55	23.5%
100	0.56	23.7%
150	0.54	26.4%
200	0.51	28.5%
300	0.45	32.4%
400	0.45	35.1%
500	0.49	34.6%

### Table B3: Site wind characteristics of Study Area B, 67.5°

<ul> <li>Normalised mean</li> <li>Turbulen</li> <li>wind speed</li> <li>intensity (<sup>6</sup></li> </ul>	0.38 25.6%	0.41 25.1%	0.43 25.0%	0.45 24.9%	0.49 23.8%	0.54 22.6%	0.62 18.9%	0.68 17.0%	700 11 92.0
Prototype scale elevation (mPD	25	50	75	100	150	200	300	400	500

57.5°	
Study Area B, 15	Turbulence intensity (%)
characteristics of S	Normalised mean wind speed
able B7: Site wind o	Prototype scale elevation (mPD)

	_	_	_	-	-	_	_	_	_
intensity (%)	15.4%	15.7%	15.3%	15.5%	16.0%	16.4%	16.9%	17.2%	706 21
wind speed	0.60	0.63	0.67	0.68	0.70	0.71	0.70	0.69	12.0
elevation (mPD)	25	50	75	100	150	200	300	400	\$00

		_	_	_	_	_	_	
17.1%	16.8%	16.7%	16.6%	16.5%	16.8%	15.0%	12.9%	10.0%
0.50	0.54	0.55	0:57	09.0	0.63	0.71	0.78	0.86
25	50	75	100-	150	200	300	400	500
	25 0.50 17.1%	25         0.50         17.1%           50         0.54         16.8%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.7%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.7%           100         0.57         16.6%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.8%           100*         0.57         16.6%           150         0.60         16.5%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.8%           100*         0.557         16.6%           150         0.63         16.5%           200         0.63         16.8%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.8%           100         0.55         16.6%           150         0.60         15.5%           200         0.63         16.8%           300         0.71         15.0%	25         0.50         17.1%           50         0.54         16.8%           75         0.55         16.7%           100         0.55         16.6%           150         0.60         16.6%           200         0.63         16.8%           300         0.71         15.0%           400         0.78         12.9%

### Table B9: Site wind characteristics of Study Area B, 202.5°

	PD) wind speed intensity (%)	0.35 25.5%	0.39 25.9%	0.40 25.5%	0.43 25.4%	0.46 25.9%	0.49 24.7%	0.56 23.3%	0.60 21.9%
--	------------------------------	------------	------------	------------	------------	------------	------------	------------	------------

ong Kong University	and Technology
The H	UU) of Scie

CLP Power Wind/Wave Tunnel Facility

AECOM Asia Co. Ltd.

3 

App A-3

, 201 • • de buie Tabla D11. City

BIL: SILE WING	characteristics of	Study Area B, 24,
Prototype scale	Normalised mean	Turbulence

	_	-	-	_	-	_	_	_	-
Turbulence intensity (%)	21.9%	22.1%	22.3%	22.5%	20.9%	17.4%	11.2%	7.2%	5.8%
Normalised mean wind speed	0,40	0.43	0.46	0.49	0.57	0.66	0.79	0.85	0.88
Prototype scale elevation (mPD)	25	50	75	100	150	200	300	400	500

0000 p .... Table B17.

ype scale	Normalised mean	Turbulence
on (mPD)	wind speed	intensity (%)
25	0.43	19.7%
50	0.47	19.5%
75	0.49	19.9%
100	0,53	19.6%
150	0.60	17.9%
200	0.66	16.1%
300	0.79	11.0%
400	0.87	7.1%
500	0.91	5.2%

19.5%	19.9%	19.6%	17.9%	16.1%	11.0%	7.1%	5.2%
0.47	0.49	0.53	09.0	0.66	0.79	0.87	0.91
50	75	100	150	200	300	400	500

The Hong Kong University of Science and Technology

·B CLP Power Wind/Wave Tunnel Facility

Table B10: Site wind characteristics of Study Area B, 225°

D

61

T

Prototype scale Normalised mean elevation (mPD) wind speed

Turbulence intensity (%) 24.4% 24.9% 23.9% 23.3% 23.3% 23.3% 11.1% 13.9% 13.9% 10.9%

0.54 0.70 0.80 0.87

25 50 75 75 75 75 75 300 500 500 500 500

0.42 0.46 0.48 0.51

Public Housing Development Kai Tak Site 1A and 1B Air Ventilation Assessment Detailed Study

64

aracteristics of ormalised mean wind speed mean 0.43 0.43 0.43 0.50 0.50 0.50 0.57 0.57 0.57 0.60 0.51 0.61 0.51 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.6
5X
ole B16: Site wind Prototype scale elevation (mPD) 25 50 100 150 200 300 200 26 150 100 160

	513: SITE WIND CHATAC	censures of Study Alea D, 2
--	-----------------------	-----------------------------

63

_				-			_		
intensity (%)	15.9%	16.0%	16.0%	16.3%	15.9%	14.7%	12.7%	10.6%	8 00%
wind speed	0.48	0.52	0.55	0.57	0.61	0.66	0.74	0.82	0.87
elevation (mPD)	25	50	75	100	150	200	300	400	\$00

e wind characteristics of Study Area E	B14: Site wind characteristics of Study Area E
e wind characteristics of Study	B14: Site wind characteristics of Study
e wind characteristics (	B14: Site wind characteristics of
e wind	B14: Site wind
	B14: Sit

\_\_\_\_

\_

Turbulence itensity (%)	17.7%	17.4%	17.3%	16.7%	15.0%	13.8%	12.0%	9.8%	7.3%
Normalised mean wind speed in	0.57	0.61	0.64	0.67	0.73	0.78	0.84	0.89	0.93
Prototype scale elevation (mPD)	25	50	75	100	150	200	300	400	500

\_

\_

## Table B15: Site wind characteristics of Study Area B, 337.5°

Prototype scale	Nonnalised mean wind speed	Turbulence intensity (%)
25	0.35	30.6%
50	0.37	31.3%
75	0.39	31.9%
100	0.40	32.5%
150	0.41	32.8%
200	0.43	33.3%
300	0.48	33.6%
400	0.51	32.7%
500	0.58	30.3%

\_

\_

\_

\_

-

ţ	
ersi	
-in	
ng l	
Š	
Bug	)
Ť	•
Ĕ	-

CLP Power Wind/Wave Tunnel Facility

AECOM Asia Co. Ltd.

·B

App A-4

The Hong Kong University of Science and Technology

•B

CLP Power Wind/Wave Tunnel Facility

## Table B17: Percentage occurrence for annual, non-typhoon directional winds at Study Area B at 150 m

		Darrantara occurra	nce for wind energy ran	.540	
Angle	0 < u < 3.3  m/s	3.3 < u ≤ 7.9 m/s	$7.9 < u \le 13.8 \text{ m/s}$	u > 13.8 m/s	Total
0,	2.0%	1.5%	0.0%	0.0%	3.5%
22.5°	0.6%	1.5%	0.3%	0.0%	2.4%
45°	2.0%	2.9%	0.0%	0.0%	5.0%
67.5°	1.1%	2.4%	0.1%	0.0%	3.5%
°06	1.1%	10.3%	6.1%	0.1%	17.5%
12.5°	3.8%	14.5%	0.9%	0.0%	19.2%
135°	6.2%	7.6%	0.1%	0.0%	13.9%
157.5°	4.8%	4.7%	0.1%	0.0%	9.6%
180°	1.9%	1.0%	0.1%	0.0%	3.0%
202.5	1.4%	1.3%	0.0%	0.0%	2.8%
225°	2.2%	1.0%	0.0%	0.0%	3.2%
247.5°	2.2%	2.4%	0.1%	0.0%	4.6%
270°	1.4%	1.8%	0.2%	0.0%	3.4%
292.5°	1.1%	1.1%	0.1%	0.0%	2.3%
315°	1.6%	1.2%	0.0%	0.0%	2.8%
337.5°	3.0%	0.4%	0.0%	0.0%	3.4%

Table B18: Percentage occurrence for summer, non-typhoon directional winds

Perce
3.3 < u ≤
0.1
0.1
0
0
5.
7.
10
4
3.1
4
2.
7.
5.
2
0.
0

CLP Power Wind/Wave Tunnel Facility

The Hong Kong University of Science and Technology

·B

Appendix B

Details of Predicted Wind Velocity Ratios (VRw)

## Appendix B Details of Predicted Wind Velocity Ratios (VR<sub>W</sub>)

"Annual Wind"

НКНА

								Wind	I Velocity F	Ratio - Annu	lal							VR <sub>w</sub> for Total
	Test Point	N	NNE	NE	ENE	E ATE	ESE	SE	SSE	S	NSS 000	MS	WSM	M	MNM	MN	MNN	6 Wind Directions
	Wind probability	0.030	0.024	C0.0	0.035	C/1.0	192	0.139	0.096	0.03	0.028	0.032	0.046	0.034	0.023	0.028	0.034	-
	P1	0.069	0.300	0.289	0.301	0.237	0.274	0.307	0.111	0.093	0.145	0.284	0.262	0.249	660.0	0.217	0.222	0.234
	P2	0.042	0.059	0.105	0.052	0.073	0.091	0.204	0.020	0.180	0.127	0.297	0.249	0.276	0.107	0.180	0.196	0.124
	Ed.	0.060	1001	0 110	0 033	0.055	0.061	0.173	0.054	0 198	0.066	0.718	0 142	0 77G	0.088	0 133	0 181	CU1 0
	22		170	1000	340.0	00100			10000	0100		0000		1210	0000	1010	101.0	0.114
	4 1	0000	001.00	160.0	617.0	001.00	th0.0		100.0	0.130		060.0	0500	101.04	0100	101.0	101.0	0.000
	£	0.038	0.041	0.018	0.019	0.03/	0.048	G17.0	0.141	0.154	161.0	0.231	1100	0.121	1.0.0	107.0	0.112	0.036
	P6	0.05/	0.156	0.092	0.08/	0.053	0.055	0.288	0.339	0.247	0.1/5	0.025	0.022	0.055	0.051	0.13/	0.191	0.133
	Ld Jd	0.040	0.142	0.140	0.200	0.221	0.166	0.106	0.308	0.274	0.108	0.249	0.056	0.077	0.150	0.183	0.122	0.170
Site 1A	P8	0.064	0.301	0.283	0.293	0.332	0.275	0.033	0.316	0.327	0.153	0.133	0.075	0.164	0.241	0.281	0.331	0.231
	6d	0.029	0.273	0.351	0.207	0.290	0.274	0.147	0.320	0.377	0.181	0.211	0.086	0.138	0.134	0.148	0.179	0.232
	P10	0.078	0.236	0.335	0.266	0.260	0.261	0.257	0.244	0.401	0.146	0.258	0.080	0.126	0.208	0.199	0.344	0.243
	D11	0 007	0 151	117	0000	0 ME	CNOO	2000	0 098	200 0	0.018	0 107	0.018	0.011	0 DEG	030	0.049	0.063
	C10	100.0	1010	0 105	1000		00100	120	0000	CVUU	1000	0.027	0.076	0000		0000	171	0000
	217	1000	0.101	0200	100.0	2010	175	1.132	200.0	740.0	170.0	7000	0.010	670.0	10000	0200	0.050	000.0
	212	0.1/4	967.0	617.0	0.101	101.0	0/1/0	0.411	0.24	0.037	190.0	610.0	190.0	0.0/0	0.000	610.0	0000	0.179
	P14	0.125	0.221	0.231	0.090	0.049	0.03/	0.352	0.151	160.0	0.224	0.2/3	0.119	0.244	0.19/	0.133	0.045	0.145
	P15	0.063	0.122	0.140	0.069	0.068	0.127	0.316	0.187	0.027	0.080	0.177	0.036	0.033	0.028	0.051	0.021	0.127
	P16	0.229	0.325	0.393	0.092	0.136	0.188	0.439	0.255	0.014	0.025	0.057	0.037	0.039	0.017	0.043	0.153	0.197
	P17	TAC O	0 333	0 404	0 135	0 141	0 184	0 246	0 102	0.063	0 160	0 228	790.0	0 193	0 130	0.061	0 131	0 179
	P18	PUC U	0.280	0310	0 190	0 117	127	0 252	0.053	7007	0.046	0.085	0.087	0.086	0.035	0.078	0.059	0 135
	010	104	00000		1000	0 150	0.05	7070	0.150	0.065	0110		0.100	1200	0440	0.145	0.000	0.120
	212	0.104	067-0	+cc.0	4070	001.0	4G0.0	417.0	001.0	con'n	0110	777.0	0.100	117.0	0.140	0.140	0.000	0.10/
	P.20	0.13/	0.229	1.39/	0.2/8	0.246	0.033	0.190	0.1/3	0.061	0.049	0.151	0.038	0.210	0.149	0.072	790.0	0.156
	P21	0.053	0.089	0.294	0.238	0.226	0.163	0.228	0.104	0.079	0.070	0.080	0.238	0.084	0.054	0.044	0.037	0.164
	P22	0.068	760.0	0.301	9920	0.238	0.224	0.38/	0.426	0.146	6/1.0	0.269	907.0	0.1/4	0.132	0.192	0.190	99770
_	P23	0.042	110.0	0.0/5	0.090	0.000	707.0	0.331	0.273	0.024	660.0	0.236	0.150	0.321	017.0	997.0	0.153	0.181
	124	0.110	101.0	0.109		Son n	701.74	007.0	117.0	0.000	410.0	0.243	0.103	417.0	0770	00770	0.004	711.0
	674	GOL O	0.048	5000	0.102	0.146	1/1/0	717.0	0.312	0.182	0.158	LCD.D	GUL.0	797.0	017.0	197.0	160.0	0.180
	P.26	0.328	0.300	0.38/	0.222	0.036	0.295	0.398	0.565	0.354	0.361	0.110	0.053	0.190	0.189	0.241	0.274	0.272
	P27	0.418	0.373	0.470	0.283	0.138	0.364	0.434	0.554	0.362	0.351	0.138	0.069	0.104	0.112	0.108	0.374	0.314
	P28	0.399	0.354	0.386	0.203	0.177	0.344	0.397	0.527	0.347	0.353	0.204	0.049	0.107	0.130	0.110	0.373	0.303
	P29	0.427	0.403	0.405	0.203	0.183	0.306	0.343	0.488	0.350	0.378	0.249	0.143	0.081	0.054	0.094	0.392	0.293
	P30	0.407	0.436	0.475	0.261	060.0	0.077	0.140	0.377	0.324	0.367	0.172	0.066	0.143	0.037	0.028	0.322	0.189
	P31	0.023	0.032	0.124	0.091	0.116	0.120	0.099	0.272	0.189	0.260	0.118	0.030	0.051	0.057	0.013	0.067	0.118
	P32	0.087	0.050	0.076	0.038	0.115	0.122	0.121	0.159	0.164	0.195	0.099	0.050	0.078	0.039	0.061	0.053	0.108
	P33	0.035	0.119	0.214	0.171	0.298	0.370	0.448	0.080	0.144	0.157	0.127	0.149	0.212	0.083	0.023	0.016	0.244
Site 1B	P34	0.024	0.192	0.228	0.123	0.174	0.319	0.249	0.033	0.124	0.089	0.136	0.040	0.094	0.079	0.042	0.043	0.170
	P35	0.012	0.137	0.183	0.110	0.111	0.140	0.163	0.025	0.182	0.152	0.125	0.091	0.171	0.086	0.067	0.016	0.116
	P36	0.022	0.060	0.301	0.185	0.211	0.281	0.190	0.039	0.160	0.252	0.152	0.268	0.269	0.137	0.038	0.008	0.187
	P37	0.036	0.024	0.285	0.181	0.240	0.289	0.225	0.172	0.281	0.398	0.172	0.227	0.268	0.145	0.076	0.027	0.218
	P38	0.046	0.043	0.120	160.0	0.180	0.236	0.264	0.352	0.378	0.338	0.052	0.188	0.240	0.277	660.0	0.104	0.211
	P39	0.122	0.159	0.267	0.177	0.062	0.108	0.232	0.248	0.191	0.124	0.082	0.129	0.233	0.109	0.124	0.102	0.150
	P40	0.031	0.067	0.196	0.079	0.194	0.166	0.077	0.169	0.121	0.186	0.095	0.054	0.043	0.054	0.066	0.060	0.129
	P41	0.072	0.102	0.190	0.121	0.160	0.044	0.065	0.146	0.178	0.135	0.088	0.080	0.086	0.147	0.139	0.107	0.108
	P42	0.04/	0.04/	0.163	0.089	0.094	0.082	790.0	0.158	0.254	0.190	0.170	0.26/	0.20/	0.255	0.1/3	0.179	0.123
	P43	1100	0.032	0.290	0.139	0.102	0.064	900.0	0.286	0.293	060.0	0.223	0.330	0.236	0.258	0.184	0.205	0.139
	P44	0.051	0.022	0.210	0.068	890.0	0/0.0	0,050	0.181	0.228	0.341	0.19/	0.15/	0.103	0.146	0.026	0.083	0.103
	C41	201.0	05010	0.100	0110	100.0	0.120	0.117	0.130	111.0	011.0	0007.0	0.173	001.0	0.000	0.070	0.100	0.102
	LVG	0 111		0 173	0400	10064	001.0	10.25	UBC U	012.0	0.202 0 768	0.334	0.367	0.178	0200	0.118	0.738	0.166
	P48	0.054	0.064	0.134	0.085	0.063	0.105	0.078	0.180	0.213	0.255	0.212	0 333	0.188	760.0	0.139	0.071	0.123
	P49	0.066	0.272	0.339	0.279	0.246	0.311	0.349	0.109	0.189	0.327	0.342	0.414	0.282	0.078	0.137	0.089	0.260
	Average SVR	0.112	0.167	0.236	0.148	0.142	0.164	0.222	0.216	0.190	0.176	0.171	0.140	0.166	0.120	0.119	0.143	0.172
	PMn	0.012	0.021	0.018	0.019	0.029	0.033	0.005	0.020	0.014	0.018	0.025	0.017	0.029	0.004	0.006	0.008	0.063
	P Max	0.427	0.436	0.475	0.301	0.332	0.370	0.448	0.565	0.401	0.398	0.342	0.417	0.426	0.277	0.281	0.392	0.314

Public Housing Development Kai Tak Site 1A and 1B Air Ventilation Assessment Detailed Study

		_									_	_			_					_			-											ř.	
VR <sub>w</sub> for Total	16 Wind Directions	0.339	0.220 0.277	0.250 0.382	0.273	0.271	0.318	0.308	0.212	0.218 0.260	0.245	0.162	0.108 0.205	0.132	0.191	0.245 0.180	0.177	0.230	0.144 0.089 0.156 0.145	0.144	0.150 0.173	0.284	0.193 0.222 0.138	0.143	0.095	0.184	0.134 0.197	0.098	0.119	0.202	0.243	0.174	0.142 0.149 0.147	0.140	0.156 0.185
	NNN 0 034	0.470	0.355	0.417 0.315	0.366	0.297	0.393	0.441	0.151	0.033	0.213	0.124	0.218	0.386	0.062	0.134 0.087	0.129	0.033	0.099	0.071	0.073	0.335	0.404	0.044	0.050	0.046	0.041	0.109	0.210	0.139	0.108	0.041	0.090	0.038	0.019
100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100	NW 0.028	0.124	0.152	0.085	0.112	0.014	0.131	0.145	0.110	0.142	0.215	0.212	0.035	0.173	0.126	0.149	0.163	0.033	0.094	0.191	0.056	0.166	0.150	0.115	0.082	0.163	0.076	0.124	0.168	0.111	0.078	0.060	0.043	0.128	0.050
	WNW 0.023	0.080	0.173	0.020 0.138	0.082	0.041	0.112	0.170	0.108	0.148	170.0	0.061	0.079	0.076	0.186	0.410	0.165	0.070	0.154 0.085 0.168 0.211	0.178	0.126	0.186	0.048 0.093	0.018	0.133	0.219	0.109	0.242	0.183	0.154	0.182	0.050	0.092	0.265	0.079
	W 0.034	0.208	0.221 0.132	0.102	0.136	0.134	0.117	0.132	0.046	0.100	0.222	0.083	0.185	0.080	0.224	0.275	0.048	0.189	0.145 0.334 0.334	0.124	0.086	0.199 0.177	0.087 0.326 0.142	0.121	0.148	0.285	0.202	0.245	0.152	0.152	0.291	0.124	0.106 0.161 0.216	0.159	0.105 0.148
	WSW 0.046	0.204	0.146 0.203	0.070 0.185	0.137	0.151	990 <sup>0</sup>	0.224	0.195	0.130	0.231	0.112	0.023	0.038	0.244	0.257	0.079	0.084	0.049 0.340 0.311	0.164	0.050	0.295	0.080 0.486 0.198	110.0	0.113	0.265	0.105	0.071	0.114	0.155	0.211	0.083	0.051	0.302	0.104
	SW 032	1.330	0.197	0.187	0.164	1234	0.174	0.278	142	0.165	0.276	0.269	0.081	0.084	0.163	0.018	0.078	0.150	0.157 0.157 0.286 0.413	0.245	0.079	0.093	0.112	0.243	115	0.288	0.221	0.089	660.0	0.086	0.095	0.178	0.057	0.042	0.127
111	028 (	474 0	268 0	378	347 0	398	.359	311 0	233	361	.139 0	.082	080 024	.053	.148 (	292 0	213 0	.168	01111	.146	.081	.025 0	.127 (	175 0	.190	233	.092	.135 0	223	174	379	283	.142 198	059 0	.175 (
o - Annual	S 03	454 0	245 0 263 0	159 0 142 0	381 0	357 0	417 0	387 0	397 0	454 0 490 0	092 0	172 0	076 0	026 0	182 0	355 0 168 0	211 0	433 0	000000000000000000000000000000000000000	152 0	200	074 0 316 0	069 0083 0	205 0	069 0	660	045 0	0 260	155 0	124 0	301 0	325 0	114 0 027 0 111	175 0 137 0	286 0 313 0
locity Rati	SE 196 0	718 0	717 0.	728 0.664 0.	511 0 570 0	697	608 0.	508 0.	165 0	039	118 0	347 0.	082 0.054 0.0	105 0	242 0	366 0.140 0.	135 0.	203	0026 104 0026	242 0	0 74 0	246 0. 373 0.	039 102 248	144 0.	167 0. 0.051	173 0	101 054 0.0	033	077 0	101	177 0.	088	203 057 0.0	143 0.0	196 0
Wind Ve	s o	0.0	9 0.0	00	00			00		00	00	3 0.	8 0.	00	0	00	0.	00		0.0	000	4 6	000		0.0	00	000		00	00	0.0	0 0 + 9		0.0	8 0.0
	013(	0.51	0.36	0.46	0.400	0.38	0.41	0.31(	0.36	0.120	0.33(	0.24	0.080	0.034	0.23!	0.192	0.14	0.16	0.211	0.18	0.20	0.25	0.32	0.19(	0.17	0.36	0.27	0.02	0.049	0.25	0.36	0.20	0.21	0.24	0.18
	6192	0.265	0.222	0.173	0.258	0.201	0.351	0.294	0.174	0.374	0.293	0.129	0.027	0.142	0.287	0.317	0.238	0.325	0.055 0.055 0.111	0.045	0.258	0.322	0.292	0.129	0.043	0.153	0.138	0.113	0.170	0.264	0.338	0.245	0.122	0.103	0.218
	0.175	0.115	0.115	0.110 0.374	0.166	0.124	0.145	0.178	0.128	0.257	0.249	0.078	0.351	0.200	0.161	0.255	0.247	0.269	0.033	0.157	0.249	0.407	0.197 0.238	0.145	0.022	0.086	0.152	0.107	0.071	0.157	0.211	0.168	0.177	0.029	0.177 0.189
	ENE 0.035	0.246	0.023	0.072	0.133	0.141	0.248	0.266	0.153	0.265	0.323	0.120	0.292	0.238	0.028	0.085	0.213	0.306	0.127 0.127 0.218	0.198	0.205	0.411	0.075 0.278	0.262	0.031	0.154	0.124	0.200	0.114	0.265	0.149	0.169	0.132 0.182 0.085	0.061	0.053
	0.05	0.470	0.124 0.282	0.139 0.115	0.234	0.428	0.438	0.480	0.389	0.427 0.476	0.349	0.181	0.450	0.142	0.125	0.044	0.254	0.424	0.081 0.201 0.285	0.149	0.19/	0.436 0.398	0.095 0.264	0.093	0.119	0.190	0.136	0.170	0.190	0.403	0.239	0.287	0.091	0.247	0.110
and the second second	0.024	0.384	0.245 0.296	0.177 0.129	0.212	0.321	0.370	0.468	0.339	0.328	0.319	0.153	0.306	0.193	0.021	0.009	0.029	0.264	0.204	0.094	0.113	0.206	0.146 0.275 0.073	0.246	0.091	0.175	0.206	0.054	0.149	0.306	0.202	0.124	0.157 0.242 0.190	0.100	0.061
1.1	0 035	0.346	0.275	0.285	0.380	0.398	0.425	0.478	0.260	0.018	0.085	0.113	0.217	0.303	0.018	0.059	0.031	0.086	0.038	0.069	0.166	0.138	0.119 0.082 0.074	0.031	0.042	0.049	0.038	0.011	0.060	0.227	0.148	0.038	0.171 0.187 0.163	0.055	0.056
	bability	Concession of the second se					0	-			(0.5		<b>.</b>	- 0	~	<b>T</b> 10	(0				~ == 1	10.00	<b>N</b> 00 0		- 0	100					_ *	*	<b>T</b> 10 (0		
	Wind pro	T1	22	T4 T5	T6	22	T10	E	11	11	T1(	T18	111 170	12	12.	12	T2(	12	2222	13.	13.1	13	13 13 13	T40	14	T4	T45	T41	T4(	150 T50	TE2	153 153	15 157 157	15	T5( T6(
			Group 1				Group 2	17				Group 3	Group 4			Group 5	-	Group 2 & 5	Group 6		Group 7		Group 8			Group 9				Group 10			Group 11	Group 12	

НКНА

App B-2

AECOM Asia Co. Ltd.

May 2011

Public Housing Development Kai Tak Site 1A and 1B Air Ventilation Assessment Detailed Study

$ \begin{array}{{ c c c c c c c c c c c c c c c c c c $				3					Wind	d Velocity F	Ratio - Annu	lal							VR <sub>w</sub> for Total
Mind probability         0.055         0.045         0.045         0.045         0.045         0.045         0.045         0.045         0.044         0.055         0.028         0.023         0.028         0.024         0.175         0.126         0.026         0.015         0.016         0.116		Test Point	z	NNE	NE	ENE	ш	ESE	SE	SSE	s	SSW	SW	MSM	M	MNM	MN	MNN	6 Wind Directions
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Wind probability	0.035	0.024	0.05	0.035	0.175	0.192	0.139	0.096	0.03	0.028	0.032	0.046	0.034	0.023	0.028	0.034	1
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		T61	0.043	0.034	0.065	0.046	0.141	0.252	0.239	0.439	0.309	0.199	0.115	0.191	0.167	0.173	0.113	0.063	0.198
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		T62	0.058	0.038	0.187	0.098	0.148	0.228	0.159	0.350	0.165	0.208	0.058	0.141	0.266	0.105	0.060	0.116	0.177
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Group 13	T63	0.105	0.072	0.219	0.054	0.110	0.106	0.087	0.409	0.407	0.381	0.045	0.285	0.402	0.384	0.200	0.183	0.181
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		T64	0.089	0.072	0.240	0.098	0.142	0.192	0.149	0.488	0.314	0.413	0.054	0.176	0.315	0.414	0.287	0.222	0.216
Tick         0.064         0.084         0.087         0.077         0.126         0.064         0.166         0.088         0.124         0.072         0.023         0.056         0.066         0.065         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.066         0.067         0.147         0.126         0.019         0.0172         0.0231         0.026         0.0166         0.066         0.0167         0.0367         0.0364         0.0164         0.0172         0.0372         0.02172         0.0372         0.0372         0.0372         0.0376         0.0172         0.0372         0.0372         0.0372         0.0372         0.0376         0.0172         0.0372         0.0272         0.0372		T65	0.010	0.107	0.212	0.180	0.181	0.156	0.047	0.158	0.247	0.210	0.129	0.256	0.220	0.345	0.202	0.188	0.160
Tion         0.155         0.166         0.166         0.166         0.145         0.143         0.224         0.221         0.032         0.154         0.251         0.205         0.205         0.205         0.205         0.205         0.205         0.205         0.205         0.205         0.102         0.118         0.172         0.182         0.166         0.172         0.172         0.172         0.172         0.172         0.102         0.118         0.172         0.125         0.173         0.126         0.173         0.126         0.173         0.126         0.172         0.126         0.127         0.127         0.127         0.127         0.127         0.127         0.126         0.127         0.126         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127		T66	0.064	0.084	0.087	0.077	0.135	0.062	0.256	0.500	0.076	0.129	0.155	0.064	0.106	0.088	0.124	0.072	0.156
Group 4         T68         0.065         0.060         0.056         0.060         0.056         0.060         0.050         0.0147         0.115         0.116         0.117         0.116         0.116         0.116         0.116         0.116         0.116         0.116         0.116         0.116         0.116         0.224         0.029         0.071         0.019         0.017         0.016         0.017         0.013         0.027         0.029         0.0210         0.0252         0.021         0.023         0.117         0.024         0.024         0.024         0.026         0.025         0.021         0.023         0.117         0.023         0.014         0.0173         0.226         0.224         0.026         0.026         0.023         0.0126         0.023         0.0126         0.023         0.0126         0.023         0.0127         0.023         0.0127         0.023         0.0127         0.023         0.023         0.0127         0.023         0.0127         0.023         0.024         0.026         0.023         0.0126         0.023         0.0177         0.0126         0.0177         0.0126         0.023         0.0177         0.023         0.0127         0.024         0.026         0.023         0.0		T67	0.159	0.166	0.186	0.145	0.149	0.268	0.292	0.242	0.209	0.321	0.221	0.032	0.154	0.261	0.215	0.505	0.223
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Group 4	T68	0.065	0.060	0.056	0.060	0.062	0.147	0.136	0.209	0.140	0.019	0.035	0.024	0.062	0.094	0.172	0.162	0.108
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		T69	0.169	0.167	0.240	0.260	0.298	0.271	0.072	0.199	0.210	0.252	0.221	0.026	0.102	0.118	0.072	0.373	0.207
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		T70	0.118	0.104	0.229	0.315	0.318	0.367	0.295	0.072	0.089	0.070	0.023	0.067	0.169	0.166	0.241	0.429	0.242
TT2         0.124         0.120         0.123         0.026         0.082         0.104         0.111         0.089         0.044         0.143         0.153         0.112         0.227         0.217         0.123         0.216         0.023         0.0140         0.118         0.117         0.126         0.226         0.233         0.0140         0.118         0.1149         0.133         0.029         0.016         0.0175         0.117         0.121         0.123         0.128         0.117         0.126         0.0216         0.016         0.0175         0.117         0.126         0.0175         0.0176         0.117         0.126         0.129         0.029         0.0176         0.177         0.120         0.123         0.029         0.0176         0.177         0.120         0.123         0.126         0.177         0.126         0.123         0.029         0.0176         0.177         0.120         0.123         0.029         0.076         0.177         0.126         0.123         0.029         0.076         0.177         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121         0.121		T71	0.241	0.190	0.103	0.224	0.207	0.329	0.397	0.660	0.228	0.190	0.149	0.093	0.096	0.179	0.234	0.326	0.290
T73         0.226         0.233         0.238         0.140         0.108         0.077         0.177         0.139         0.135         0.126         0.217         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.127         0.126         0.126         0.126         0.127         0.126         0		172	0.124	0.120	0.122	0.082	0.054	0.088	0.104	0.191	0.111	0.089	0.044	0.143	0.168	0.053	0.112	0.227	0.107
TT4         0.026         0.082         0.024         0.047         0.065         0.157         0.256         0.312         0.117         0.139         0.156         0.175         0.175         0.120           T75         0.063         0.008         0.101         0.194         0.163         0.173         0.343         0.290         0.118         0.116         0.077         0.779         0.779         0.201           T76         0.063         0.008         0.101         0.109         0.194         0.163         0.177         0.343         0.290         0.118         0.179         0.012           T77         0.103         0.061         0.345         0.299         0.177         0.134         0.126         0.179         0.129         0.121		173	0.226	0.233	0.238	0.140	0.108	0.070	0.173	0.112	0.104	0.187	0.149	0.133	0.029	0.020	0.065	0.217	0.127
Group 15         T75         0.106         0.073         0.334         0.225         0.194         0.163         0.177         0.340         0.343         0.230         0.116         0.037         0.076         0.179         0.201           T76         0.063         0.010         0.101         0.193         0.096         0.177         0.164         0.112         0.123         0.126         0.037         0.075         0.072         0.072         0.129           T77         0.103         0.061         0.345         0.299         0.177         0.164         0.112         0.123         0.125         0.091         0.029         0.072         0.082         0.072         0.18         0.171         0.166         0.234         0.255         0.374         0.228         0.206         0.173         0.166         0.129         0.121		T74	0.026	0.066	0.082	0.024	0.047	0.065	0.157	0.295	0.312	0.117	0.139	0.156	0.121	0.138	0.158	0.175	0.120
TT6         0.063         0.008         0.101         0.109         0.119         0.096         0.177         0.128         0.093         0.236         0.142         0.142         0.150         0.092         0.082         0.072         0.128           T77         0.103         0.061         0.345         0.259         0.179         0.213         0.128         0.098         0.236         0.125         0.099         0.026         0.039         0.029         0.089         0.029         0.018         0.178         0.128         0.098         0.236         0.175         0.029         0.089         0.029         0.018         0.012         0.012         0.128         0.039         0.128         0.039         0.176         0.029         0.089         0.128         0.024         0.129         0.017         0.021         0.018         0.021         0.021         0.011         0.012         0.012         0.011         0.012         0.021         0.012         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021         0.021 </td <td>Group 15</td> <td>175</td> <td>0.106</td> <td>0.073</td> <td>0.334</td> <td>0.225</td> <td>0.194</td> <td>0.163</td> <td>0.173</td> <td>0.360</td> <td>0.340</td> <td>0.343</td> <td>0.290</td> <td>0.118</td> <td>0.116</td> <td>0.037</td> <td>0.076</td> <td>0.179</td> <td>0.201</td>	Group 15	175	0.106	0.073	0.334	0.225	0.194	0.163	0.173	0.360	0.340	0.343	0.290	0.118	0.116	0.037	0.076	0.179	0.201
T77         0.103         0.061         0.345         0.297         0.259         0.179         0.228         0.264         0.125         0.091         0.029         0.089         0.181           T78         0.065         0.072         0.188         0.717         0.228         0.204         0.039         0.067         0.072         0.077         0.037         0.077         0.037         0.077         0.037         0.027         0.121         0.121         0.128         0.121         0.129         0.129         0.037         0.027         0.129         0.037         0.027         0.129         0.037         0.027         0.129         0.129         0.037         0.029         0.129         0.129         0.037         0.203         0.129         0.037         0.233         0.127         0.265         0.374         0.239         0.177         0.127         0.233         0.127         0.263         0.039         0.174         0.274         0.233         0.170         0.129         0.374         0.233           Average LVR         0.128         0.189         0.286         0.239         0.2019         0.140         0.170         0.170         0.120         0.171         0.201         0.203 <t< td=""><td></td><td>176</td><td>0.063</td><td>0.008</td><td>0.101</td><td>0.109</td><td>0.119</td><td>960.0</td><td>0.177</td><td>0.164</td><td>0.112</td><td>0.123</td><td>0.150</td><td>0.142</td><td>0.150</td><td>0.092</td><td>0.082</td><td>0.072</td><td>0.121</td></t<>		176	0.063	0.008	0.101	0.109	0.119	960.0	0.177	0.164	0.112	0.123	0.150	0.142	0.150	0.092	0.082	0.072	0.121
T78         0.065         0.099         0.066         0.058         0.092         0.092         0.0157         0.255         0.334         0.228         0.234         0.277         0.035         0.027         0.057         0.0121           Average         0.192         0.0162         0.160         0.178         0.171         0.6696         0.239         0.252         0.307         0.137         0.027         0.037         0.037         0.037         0.037         0.031         0.041         0.023         0.041         0.031         0.017         0.031         0.011         0.017         0.017         0.017         0.011         0.011         0.012         0.011         0.011         0.012         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.012         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011         0.011 <td< td=""><td></td><td>177</td><td>0.103</td><td>0.061</td><td>0.345</td><td>0.297</td><td>0.259</td><td>0.179</td><td>0.213</td><td>0.128</td><td>0.098</td><td>0.236</td><td>0.264</td><td>0.126</td><td>0.125</td><td>0.091</td><td>0.029</td><td>0.089</td><td>0.188</td></td<>		177	0.103	0.061	0.345	0.297	0.259	0.179	0.213	0.128	0.098	0.236	0.264	0.126	0.125	0.091	0.029	0.089	0.188
T79 0.192 0.095 0.072 0.188 0.178 0.178 0.314 0.471 0.696 0.239 0.262 0.307 0.139 0.177 0.032 0.054 0.374 0.293 Average LVR 0.128 0.168 0.232 0.160 0.152 0.181 0.229 0.245 0.200 0.189 0.170 0.144 0.153 0.126 0.170 0.171 0.1 T <sub>Ma</sub> 0.010 0.008 0.044 0.023 0.017 0.027 0.028 0.033 0.019 0.019 0.018 0.026 0.018 0.014 0.014 0.019 0.01 T <sub>Mas</sub> 0.478 0.468 0.480 0.411 0.407 0.453 0.586 0.742 0.490 0.474 0.443 0.486 0.402 0.414 0.287 0.505 0.019		T78	0.065	660.0	0.066	0.058	0.082	0.092	0.157	0.255	0.374	0.228	0.204	0.039	0.107	0.035	0.020	0.057	0.121
Average LVR 0.128 0.168 0.232 0.160 0.152 0.181 0.229 0.245 0.200 0.189 0.170 0.144 0.163 0.126 0.120 0.171 0. T <sub>Me</sub> 0.010 0.008 0.044 0.023 0.017 0.027 0.028 0.033 0.019 0.019 0.018 0.028 0.018 0.014 0.014 0.019 0.01 T <sub>Mes</sub> 0.478 0.468 0.480 0.411 0.407 0.453 0.586 0.742 0.490 0.474 0.443 0.486 0.402 0.414 0.287 0.505 0.01		179	0.192	0.095	0.072	0.188	0.178	0.314	0.471	0.696	0.239	0.262	0.307	0.139	0.127	0.032	0.054	0.374	0.293
T <sub>Me</sub> 0.010 0.008 0.044 0.023 0.017 0.028 0.033 0.019 0.019 0.018 0.028 0.030 0.019 0.018 0.026 0.018 0.014 0.019 0.0 T <sub>Mee</sub> 0.478 0.468 0.480 0.411 0.407 0.453 0.586 0.742 0.490 0.474 0.443 0.486 0.402 0.414 0.287 0.505 0.0		Average LVR	0.128	0.168	0.232	0.160	0.152	0.181	0.229	0.245	0.200	0.189	0.170	0.144	0.163	0.126	0.120	0.171	0.183
T Max 0.478 0.468 0.480 0.411 0.407 0.453 0.586 0.742 0.490 0.474 0.443 0.486 0.402 0.414 0.287 0.505 0.3	2	TMn	0.010	0.008	0.044	0.023	0.017	0.027	0.028	0.033	0.019	0.019	0.018	0.023	0.026	0.018	0.014	0.019	0.061
		T Max	0.478	0.468	0.480	0.411	0.407	0.453	0.586	0.742	0.490	0.474	0.443	0.486	0.402	0.414	0.287	0.505	0.382

Remarks: Test Point T45, T46, T52 and T53 are located at 2m above the top of the commerical centre or carport.

## Appendix B Details of Predicted Wind Velocity Ratios (VR<sub>W</sub>)

НКНА

"Summer Season"

	S	Т			-							_	Ť		-		T		_	Ē	-		1			Ť						Ť						<u> </u>
VR <sub>w</sub> for Total	16 Wind Direction	-	0.356	0.283	0.371	0.276	0.276	0.318	0.293	0.155	0.218	0.186 0.244	0.228	0.306 0.168	0.080	0.088	0.209	0.269	0.175	0.199	0.170	0.171	0.159	0.135	0231	0170	0.170	0.147	0.068	0.227	0.182	0.172	0.119	0.155	0.249	0.185 0.174	0.128 0.136	0.171 0.096 0.158
	NNN	0.014	0.355	0.453	0.315	0.366	0.297	0.261	0.393	0.179	0.151	0.033	0.213	0.184	0.218	0.386	0.062	0.134	0.087	0.033	0.062	0.153	0.071	0.073	0.335	160.0	0.161	0.044	0.037	0.046	0.119	0.099	0.210	0.186	0.108	0.043	0.090 0.125	0.038
	NW	110.0	0.124	0.198	0.058	0.112	0.014	0.210	0.131	0.110	0.110	0.142	0.215	0.212	0.035	0.173	0.126	0.149	0.060	0.033	0.030	0.094	0.191	0.056	0.166	0.275	0.150	0.115	0.047	0.163	0.149	0.124	0.168	0.064	0.078	0.032	0.043 0.029 0.023	0.033
	MNM	0.04	0.080	0.182	0.138	0.082	0.041	0.083	0.112	0.038	0.108	0.148	0.077	0.240	6/0.0	0.076	0.186	0.410	0.251	0.070	0.154	0.168	0.178	0.126	0.186	0.048	0.093	0.018	0.025	0.219	0.109	0.242	0.183	0.092	0.182	0.093	0.041 0.092	0.115
	M	0.084	0.208	0.132	0.154	0.136	0.134	0.107	0.137	0.046	0.052	0.121	0.222	0.361	0.185	0.080	0.224	0.275	0.255	0.189	0.271	0.334	0.124	0.086	0.199	0.087	0.326	0.121	0.100	0.285	0.162	0.236	0.152	0.102	0.291	0.046	0.106 0.161 0.216	0.159 0.140 0.105
	WSM	171.0	0.146	0.203	0.185	0.137	0.151	0.205	0.004	0.102	0.195	0.130	0.231	0.382	0.023	0.038	0.244	0.257	0.114	0.084	0.148	0.340	0.164	0.065	0.295	0.080	0.486	110.0	0.040	0.265	0.205	0.192	0.114	0.137	0.211	0.074 0.083	0.051 0.088 0.137	0.302 0.167 0.104
1.2100	SW SW	0.012	0.330	0.262	0.360	0.164	0.234	0.230	0.778	0.142	0.190	0.165 0.283	0.276	0.366	0.081	0.084	0.163	0.018	0.037	0.150	0.102	0.286	0.245	0.084	0.093	0 117	0.195	0.243	0.115	0.288	0.221	0.089	660.0	0.088	0.095	0.085 0.178	0.057 0.217 0.168	0.042
eason	SSW	0.010	0.268	0.236	0.378	0.347	0.398	0.408	0.359	0.255	0.233	0.167 0.361	0.139	0.269	0.080	0.053	0.148	0.292	0.152	0.168	0.069	0.074	0.146	0.112	0.025	107.0	0.150	0.175	0.035	0.233	0.092	0.135	0.223	0.171	0.195	0.379	0.053 0.142 0.198	0.123
Summer S	S	690.0	0.245	0.263	0.142	0.381	0.357	0.428	0.41/	0.286	0.397	0.454	0.092	0.045	0.076	0.026	0.182	0.355	0.168	0.433	0.157	0.087	0.152	0.339	0.074	010.0	0.083	0.205	0.055	660.0	0.019	190.0	0.155	0.137	0.301	0.450 0.325	0.114 0.027 0.111	0.175 0.137 0.286
city Ratio -	SSE	0.089	0.294	0.717	0.664	0.511	0.597	0.742	0.508	0.222	0.165	0.039	0.118	0.302	0.082	0.105	0.242	0.366	0.140	0.203	0.195	0.104	0.242	0.311	0.246	01030	0.102	0.144	0.051	0.173	0.054	0.033	170.0	0.159	0.177	0.339	0.203 0.057 0.726	0.190
Wind Velo	SE	0.13	0.366	0.381	0.586	0.406	0.385	0.419	0.316	0.179	0.366	0.120	0.330	0.419 0.243	0.072	0.034	0.235	0.278	0.192	0.166	0.286	0.070	0.182	0.068	0.254	0 325	0.284	0.190	0.124	0.361	0.272	0.028	0.049	0.255	0.361	0.224	0.227 0.210 0.148	0.241 0.066 0.182
	ESE	0.114	0.265	0.184	0.453	0.258	0.201	0.302	0.351	0.156	0.174	0.374 0.186	0.293	0.318 0.129	0.027	0.142	0.287	0.317	0.250	0.325	0.151	0.111	0.045	0.091	0.322	101.0	0.222	0.129	0.031	0.153	0.259	0.1/1 0.113	0.170	0.165	0.338	0.114 0.245	0.122 0.123 0.092	0.103 0.059 0.218
	E	0.083	0.115	0.130	0.374	0.166	0.124	0.075	0.145	0.071	0.128	0.257	0.249	0.164 0.078	0.072	0.200	0.161	0.255	0.247	0.269	0.095	0.219	0.157	0.238	0.407	10101	0.238	0.145	0.058	0.086	0.227	0.198	0.071	0.058	0.211	0.121 0.168	0.177 0.142 0.141	0.029
	ENE	0.008	0.246	0.089	0.304	0.133	0.141	0.306	0.248	0.153	0.164	0.265	0.323	0.256 0.120	0.292	0.238	0.028	0.085	0.093	0.306	0.038	0.218	0.198	0.222	0.411	0.075	0.278	0.262	0.046	0.154	0.249	0.1/9	0.114	0.250	0.149	0.146 0.169	0.132 0.182 0.085	0.082
1111	NE	0.000	0.470	0.282	0.115	0.234	0.428	0.411	0.438	0.366	0.389	0.427 0.476	0.349	0.302 0.181	0.450	0.142	0.125	0.044	0.121	0.424	0.061	0.201	0.149	0.197	0.436	0.095	0.264	0.093	0.082	0.190	0.130	0.205	0.190	0.378	0.239	0.322 0.287	0.091 0.379 0.369	0.061
	NNE	0.003	0.245	0.296	0.129	0.212	0.321	0.265	0.370	0.339	0.412	0.328 0.319	0.319	0.206	0.306	0.193	0.021	60000	0.029	0.264	0.054	0.204	0.094	0.113	0.206	0146	0.275	0.246	0.061	0.175	0.206	0.148	0.149	0.310	0.202	0.299	0.157 0.242 0.190	0.100
	N	0.008	0.346	0.334	0.267	0.380	0.398	0.367	0.425	0.114	0.260	0.018	0.085	0.085 0.113	0.217	0.159	0.018	0.059	0.050	0.086	0.056	0.042	0.069	0.083	0.138	0.119	0.082	0.031	0.023	0.049	0.067	0.046	0.060	0.232	0.148	0.154 0.038	0.171 0.187 0.163	0.055
	Test Point	vvind probability	12	13	14 T5	T6 T7	T8	T9	T110	T12	T13	T14 T15	T16	T17 T18	119	121	123	T24	125 126	727	T28 T29	130	132	T33 T34	135 135	130	138 139	T40	T42	143	144 T45	146 T47	T48	T49 T50	T51	152 153	T54 T55 T56	157 158 159
		12		Group 1					Group 2					Group 3	, may	theore			Group 5	Group 2 & 5	Gmin 6			Gmin 7	- droip		Group 8			Group 9				Gmin 10	a doop		Group 11	Group 12

Public Housing Development Kai Tak Site 1A and 1B Air Ventilation Assessment Detailed Study

_	6				(*************************************	i			Í	r		r		
VR <sub>w</sub> for Total	16 Wind Directions	0.356 0.237 0.283 0.250 0.371	0.276 0.244 0.218 0.318 0.318 0.293 0.293 0.156 0.156 0.156 0.156 0.218	0.228 0.306 0.168	0.080 0.145 0.088 0.150	0.209 0.269 0.175 0.152	0.199	0.170 0.106 0.171 0.195	0.159 0.135 0.142 0.231 0.238	0.170 0.245 0.170	0.147 0.126 0.068 0.127 0.140 0.182 0.182	0.099 0.119 0.155 0.178 0.249 0.178 0.174	0.128 0.136 0.150	0.171 0.096 0.158 0.158
	0.014	0.470 0.355 0.453 0.417 0.315	0.366 0.245 0.245 0.261 0.261 0.393 0.441 0.441 0.179 0.179 0.151 0.033	0.213 0.184 0.124	0.218 0.391 0.386 0.487	0.062 0.134 0.087 0.129	0.033	0.062 0.099 0.153 0.075	0.071 0.073 0.112 0.335 0.337	0.404 0.177 0.161	0.044 0.050 0.037 0.046 0.041 0.119 0.099	0.109 0.210 0.186 0.139 0.108 0.043 0.041	0.090 0.125 0.146	0.097 0.038 0.019
	0.017	0.124 0.152 0.198 0.085 0.058	0.112 0.021 0.014 0.131 0.131 0.145 0.110 0.110 0.1142 0.1142	0.215 0.224 0.212	0.035 0.170 0.173 0.237	0.126 0.149 0.060 0.163	0.033	0.030 0.115 0.094 0.101	0.191 0.056 0.118 0.166 0.285	0.150	0.115 0.082 0.047 0.163 0.163 0.149 0.149	0.124 0.168 0.064 0.078 0.078 0.032 0.060	0.043 0.029 0.023	0.128 0.033 0.050 0.055
	WNW 0.04	0.080 0.173 0.182 0.182 0.020 0.138	0.082 0.033 0.041 0.112 0.112 0.170 0.170 0.170 0.168 0.160	0.077 0.240 0.061	0.079 0.140 0.076 0.108	0.186 0.410 0.251 0.165	0.070	0.154 0.085 0.168 0.211	0.178 0.126 0.115 0.186 0.126	0.048 0.093 0.051	0.018 0.133 0.255 0.219 0.219 0.172 0.172	0.242 0.183 0.192 0.154 0.182 0.093 0.050	0.041 0.092 0.094	0.265 0.115 0.077 0.079
8	W 0.084	0.208 0.221 0.132 0.154	0.136 0.055 0.134 0.107 0.117 0.117 0.132 0.132 0.132 0.132 0.132 0.121	0.222 0.361 0.083	0.185 0.259 0.080 0.100	0.224 0.275 0.255 0.048	0.189	0.271 0.145 0.334 0.334	0.124 0.086 0.026 0.199 0.177	0.087 0.326 0.142	0.121 0.148 0.100 0.285 0.285 0.162 0.162 0.236	0.245 0.152 0.162 0.162 0.152 0.291 0.291 0.246 0.124	0.106 0.161 0.216	0.159 0.140 0.105 0.105 0.148
	WSW 0.127	0.204 0.146 0.203 0.070 0.185	0.137 0.151 0.151 0.205 0.205 0.205 0.205 0.205 0.205 0.102 0.195 0.195 0.148	0.231 0.382 0.112	0.023 0.100 0.038 0.045	0.244 0.257 0.114 0.079	0.084	0.148 0.049 0.340 0.411	0.164 0.065 0.050 0.295 0.295	0.080 0.486 0.198	0.077 0.113 0.040 0.265 0.105 0.105 0.192	0.071 0.114 0.137 0.155 0.155 0.074 0.074 0.083	0.051 0.088 0.132	0.302 0.167 0.104 0.189
	SW 0.072	0.330 0.197 0.262 0.187 0.360	0.164 0.187 0.234 0.230 0.174 0.174 0.142 0.190 0.190 0.165 0.283	0.276 0.366 0.269	0.081 0.056 0.084 0.088	0.163 0.018 0.037 0.078	0.150	0.102 0.157 0.286 0.413	0.245 0.084 0.079 0.093 0.443	0.112 0.417 0.195	0.243 0.221 0.115 0.115 0.149 0.221 0.221	0.089 0.099 0.086 0.095 0.095 0.085 0.178	0.057 0.217 0.168	0.115 0.042 0.077 0.177
Season	0.076	0.474 0.268 0.268 0.236 0.181 0.378	0.347 0.343 0.348 0.398 0.369 0.311 0.355 0.355 0.255 0.255 0.255 0.255 0.267 0.267	0.139 0.269 0.082	0.080 0.024 0.053 0.120	0.148 0.292 0.152 0.213	0.168	0.069 0.111 0.074 0.083	0.146 0.112 0.081 0.025 0.257	0.127 0.150 0.129	0.175 0.190 0.035 0.233 0.110 0.110 0.142	0.135 0.223 0.171 0.174 0.195 0.379 0.283	0.053 0.142 0.198	0.059 0.123 0.175 0.175
- Summer	0.069	0.454 0.245 0.263 0.159 0.142	0.381 0.312 0.357 0.357 0.357 0.357 0.357 0.387 0.387 0.387 0.387 0.397 0.397	0.092 0.045 0.172	0.076 0.023 0.026 0.091	0.182 0.355 0.168 0.211	0.433	0.157 0.059 0.087 0.146	0.152 0.339 0.200 0.074 0.316	0.069 0.083 0.219	0.205 0.069 0.055 0.099 0.045 0.019	0.093 0.155 0.137 0.124 0.301 0.450 0.325	0.114 0.027 0.111	0.175 0.137 0.286 0.313
ocity Ratio	SSE 0.089	0.718 0.294 0.717 0.728 0.728 0.664	0.511 0.570 0.577 0.597 0.508 0.508 0.508 0.508 0.222 0.165 0.165 0.300	0.118 0.302 0.347	0.082 0.054 0.105 0.261	0.242 0.366 0.140 0.135	0.203	0.195 0.056 0.104 0.204	0.242 0.311 0.074 0.246 0.373	0.102	0.144 0.167 0.051 0.173 0.101 0.054 0.061	0.033 0.077 0.159 0.101 0.177 0.339 0.088	0.203 0.057 0.226	0.190 0.143 0.196 0.178
Wind Vel	SE 0.19	0.512 0.366 0.381 0.463 0.586	0.406 0.365 0.385 0.419 0.418 0.418 0.418 0.418 0.179 0.179 0.179 0.120	0.330 0.419 0.243	0.072 0.088 0.034 0.328	0.235 0.278 0.192 0.143	0.166	0.286 0.218 0.070 0.103	0.182 0.068 0.204 0.254 0.254	0.325 0.214 0.284	0.190 0.177 0.124 0.361 0.229 0.272 0.272	0.028 0.049 0.255 0.255 0.252 0.252 0.224 0.226	0.227 0.210 0.148	0.241 0.066 0.182 0.178
	ESE 0.114	0.265 0.222 0.173 0.173 0.453	0.258 0.239 0.201 0.351 0.351 0.351 0.351 0.351 0.351 0.374 0.374	0.293 0.318 0.129	0.027 0.289 0.142 0.043	0.287 0.317 0.250 0.238	0.325	0.151 0.055 0.111 0.116	0.045 0.091 0.258 0.322 0.167	0.222 0.222 0.059	0.129 0.043 0.031 0.153 0.153 0.138 0.138	0.113 0.170 0.165 0.165 0.264 0.338 0.338 0.245	0.122 0.123 0.092	0.103 0.059 0.218 0.261
	0.083	0.115 0.115 0.130 0.110 0.110 0.374	0.166 0.129 0.124 0.178 0.178 0.178 0.178 0.178 0.178 0.257 0.257	0.249 0.164 0.078	0.072 0.351 0.200 0.040	0.161 0.255 0.259 0.247	0.269	0.095 0.033 0.219 0.050	0.157 0.238 0.249 0.407 0.151	0.197 0.238 0.017	0.145 0.022 0.058 0.086 0.152 0.152	0.107 0.071 0.058 0.157 0.157 0.157 0.157 0.157	0.177 0.142 0.141	0.029 0.026 0.177 0.189
	ENE 0.008	0.246 0.023 0.089 0.072 0.304	0.133 0.052 0.141 0.306 0.248 0.266 0.153 0.164 0.164 0.265	0.323 0.256 0.120	0.292 0.382 0.238 0.090	0.028 0.085 0.093 0.213	0.306	0.038 0.127 0.218 0.063	0.198 0.222 0.205 0.411 0.227	0.075 0.278 0.044	0.262 0.031 0.046 0.154 0.154 0.124 0.124	0.200 0.114 0.250 0.265 0.149 0.146 0.169	0.132 0.182 0.085	0.051 0.082 0.053 0.151
	0.006	0.470 0.124 0.282 0.139 0.115	0.234 0.376 0.478 0.411 0.418 0.480 0.480 0.366 0.389 0.389 0.476	0.349 0.302 0.181	0.450 0.273 0.142 0.099	0.125 0.044 0.121 0.254	0.424	0.061 0.081 0.201 0.285	0.149 0.197 0.123 0.436 0.398	0.264	0.093 0.119 0.190 0.136 0.136 0.259	0.170 0.190 0.378 0.403 0.239 0.322 0.322	0.091 0.379 0.269	0.247 0.061 0.110 0.220
	0.003	0.384 0.245 0.296 0.177 0.129	0.212 0.279 0.321 0.370 0.468 0.339 0.339 0.319 0.319	0.319 0.206 0.153	0.306 0.094 0.193 0.329	0.021 0.009 0.046 0.029	0.264	0.054 0.074 0.204 0.114	0.094 0.113 0.078 0.206 0.328	0.146 0.275 0.073	0.246 0.091 0.061 0.175 0.175 0.206 0.206	0.054 0.149 0.310 0.306 0.202 0.299 0.124	0.157 0.242 0.190	0.100 0.060 0.061 0.012
	N 0.008	0.346 0.275 0.334 0.285 0.285 0.267	0.380 0.384 0.398 0.367 0.478 0.478 0.114 0.118 0.118 0.113	0.085 0.085 0.113	0.217 0.120 0.159 0.303	0.018 0.059 0.050 0.031	0.086	0.056 0.038 0.042 0.019	0.069 0.083 0.166 0.138 0.267	0.119 0.082 0.074	0.031 0.042 0.049 0.049 0.067 0.067	0.011 0.060 0.232 0.227 0.154 0.154 0.038	0.171 0.187 0.163	0.112 0.055 0.056 0.056
	Vind probability	T75575	T6 17 110 111 111 112 113 115 115	T16 T17 T18	119 121 122	T23 T24 T25	127	T28 T29 T30	T32 T33 T34 T35	137 138 139	T40 T41 T42 T44 T45	T47 T48 T50 T51 T52 T53	T54 T55 T56	157 158 159 160
		Group 1	Group 2	Group 3	Group 4	Group 5	Group 2 & 5	Group 6	Group 7	Group 8	Group 9	Group 10	Group 11	Group 12

May 2011

НКНА

Public Housing Development Kai Tak Site 1A and 1B Air Ventilation Assessment Detailed Study

НКНА

					101 - 111 - 101 - 101		and second s	Wind Velo	ocity Ratio	- Summer	eason	Contraction of the second	in the subscription				- Province - State	VR <sub>w</sub> for Total
	Test Point	N	NNE	NE	ENE	ш	ESE	SE	SSE	S	SSW	SW	MSM	M	MNM	MN	MNN	16 Wind Directions
	Wind probability	0.008	0.003	0.006	0.008	0.083	0.114	0.19	0.089	0.069	0.076	0.072	0.127	0.084	0.04	0.017	0.014	1
	T61	0.043	0.034	0.065	0.046	0.141	0.252	0.239	0.439	0.309	0.199	0.115	0.191	0.167	0.173	0.113	0.063	0.219
1000 C	T62	0.058	0.038	0.187	0.098	0.148	0.228	0.159	0.350	0.165	0.208	0.058	0.141	0.266	0.105	0.060	0.116	0.181
Group 13	T63	0.105	0.072	0.219	0.054	0.110	0.106	0.087	0.409	0.407	0.381	0.045	0.285	0.402	0.384	0.200	0.183	0.228
	T64	0.089	0.072	0.240	0.098	0.142	0.192	0.149	0.488	0.314	0.413	0.054	0.176	0.315	0.414	0.287	0.222	0.239
	T65	0.010	0.107	0.212	0.180	0.181	0.156	0.047	0.158	0.247	0.210	0.129	0.256	0.220	0.345	0.202	0.188	0.172
	T66	0.064	0.084	0.087	0.077	0.135	0.062	0.256	0.500	0.076	0.129	0.155	0.064	0.106	0.088	0.124	0.072	0.163
	T67	0.159	0.166	0.186	0.145	0.149	0.268	0.292	0.242	0.209	0.321	0.221	0.032	0.154	0.261	0.215	0.505	0.217
Group 4	T68	0.065	0.060	0.056	0.060	0.062	0.147	0.136	0.209	0.140	0.019	0.035	0.024	0.062	0.094	0.172	0.162	660.0
	T69	0.169	0.167	0.240	0.260	0.298	0.271	0.072	0.199	0.210	0.252	0.221	0.026	0.102	0.118	0.072	0.373	0.165
	170	0.118	0.104	0.229	0.315	0.318	0.367	0.295	0.072	0.089	0.070	0.023	0.067	0.169	0.166	0.241	0.429	0.188
	T71	0.241	0.190	0.103	0.224	0.207	0.329	0.397	0.660	0.228	0.190	0.149	0.093	960.0	0.179	0.234	0.326	0.270
	172	0.124	0.120	0.122	0.082	0.054	0.088	0.104	0.191	0.111	0.089	0.044	0.143	0.168	0.053	0.112	0.227	0.111
	173	0.226	0.233	0.238	0.140	0.108	0.070	0.173	0.112	0.104	0.187	0.149	0.133	0.029	0.020	0.065	0.217	0.121
	T74	0.026	0.066	0.082	0.024	0.047	0.065	0.157	0.295	0.312	0.117	0.139	0.156	0.121	0.138	0.158	0.175	0.149
Group 15	175	0.106	0.073	0.334	0.225	0.194	0.163	0.173	0.360	0.340	0.343	0.290	0.118	0.116	0.037	0.076	0.179	0.205
	176	0.063	0.008	0.101	0.109	0.119	0.096	0.177	0.164	0.112	0.123	0.150	0.142	0.150	0.092	0.082	0.072	0.136
	777	0.103	0.061	0.345	0.297	0.259	0.179	0.213	0.128	860.0	0.236	0.264	0.126	0.125	0.091	0.029	0.089	0.175
	178	0.065	660.0	0.066	0.058	0.082	0.092	0.157	0.255	0.374	0.228	0.204	0.039	0.107	0.035	0.020	0.057	0.146
	T79	0.192	0.095	0.072	0.188	0.178	0.314	0.471	0.696	0.239	0.262	0.307	0.139	0.127	0.032	0.054	0.374	0.300
	Average LVR	0.128	0.168	0.232	0.160	0.152	0.181	0.229	0.245	0.200	0.189	0.170	0.144	0.163	0.126	0.120	0.171	0.185
	T <sub>Min</sub>	0.010	0.008	0.044	0.023	0.017	0.027	0.028	0.033	0.019	0.019	0.018	0.023	0.026	0.018	0.014	0.019	0.068
	T Max	0.478	0.468	0.480	0.411	0.407	0.453	0.586	0.742	0.490	0.474	0.443	0.486	0.402	0.414	0.287	0.505	0.371

Test Point T45, T46, T52 and T53 are located at 2m above the top of the commerical centre or carport.

Appendix C

Average  $\text{VR}_{\text{W}}$  Result for Individual Test Points and Different Test Points Groups under Different Wind Directions

# Average VRw Result for Individual Test Points and Different Test Points Groups under Different Wind Directions Appendix C

НКНА















-

VRw Plot for Overall Test Points







Tripidation (1997) 1992 - 199

AECOM Asia Co. Ltd.

VRw Plot for Perimeter Test Points



Indalla

282 0.05







VRw Plot for Overall Test Points





VRw Plot for Perimeter Test Points

ı٩



НКНА













- -

000 0.175 0.

-







VRw Plot for Overall Test Points

VRw Result under S Wind Direction

AECOM Asia Co. Ltd.

НКНА



НКНА













ألالمي

обрание и стание и С стание и стание

VRw Plot for Perimeter Test Points

НКНА



VRs 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.07 0.07 0.07 0.07 0.07 0.05

VRw Plot for Overall Test Points









VRw Plot for Perimeter Test Points

НКНА









Appendix D

Wind Velocity Ratio Contour and Vector Plots at 2m above Ground under Different Wind Directions





0.6

0.8

0.7

0.5

0.4

Wind Velocity Ratio Contour Plat at 2m above Ground

Wind Velocity Vector Plat at 2m above Ground

НКНА



"ENE"

AECOM Asia Co. Ltd.

"JN.,

0.7

0.5

0.4

0.6

0.3

0.2

0.0



AECOM Asia Co. Ltd.

May 2011

НКНА

Ļ

"SE"

НКНА



"SSE"

May 2011

0.7

0.6

0.5

0.4

0.3

0.2

0.0



"MSS",

AECOM Asia Co. Ltd.

يْ

...NS,,,

НКНА

0.7

0.6

0.5

0.3

0.4

0.2

0.0



"MSM,,

0.7

0.6

0.5

0.3

0.4

0.2

0.0



..MNM,,

AECOM Asia Co. Ltd.

۰.Λ,

0.7

0.6

0.5

0.4



..MNN,,

0.0

НКНА

"WW"

AECOM Asia Co. Ltd.

App D-8

May 2011